

## **8 Description of schematic circuit of heat removal from the core, target and other elements of SAD.**

8.1 The blanket and target are cooled by closed-loop forced circulation of air coolant through the core, target and other elements of the loop 1 (Figure 8.1). The coolant flow through the core is organized top-down. The circuit given in Figure 8.1 was developed in collaboration with FSUE GSPI (State Special Project Institute) and it is proposed for implementation in the SAD installation project. Schematic solutions given below are considered in chapter 12 at safety analysis of the SAD.

8.2 The cooling system includes two gear-type compressors of type 34VF - 37/1 (items A 5/1 and A 5/2), two air cooling devices (heat exchanger of loop 1) of type AVM-9-06-BZ-N (items 2-1 and 2-2) and one air cooling device of loop 2 (heat exchanger of loop 2) of type AVM-20-06-B1-N (item 4), piping, locking and regulating armature and a number of auxiliary systems.

8.3 The pressure in loop 1 is maintained by volume change compensation system called gasholder, which is connected to loop 1 at the suck-in part of the compressor. Working pressure of coolant in the gasholder amounts to  $\sim 0,1$  MPa.

8.4 The compressor provides for a prescribed coolant flow rate through the core and target (excess air circulates through by-pass line  $D_{\text{pass}} = 80$  mm). At the expense of compression, the coolant temperature at the output of compressor raises up to  $\sim 90^{\circ}\text{C}$ , that is why the coolant travels, through the pipe line of  $D_{\text{pass}} = 200$  mm to heat exchanger 2-2, where it is cooled to temperature  $\sim 42^{\circ}\text{C}$ , after that the coolant flows through pipeline  $D_{\text{pass}} 200$  mm to blanket and target of SAD.

8.5 Before entrance to SAD, coolant flow is divided in two flows: the greater part of the coolant flows, through the pipeline  $D_{\text{pass}}200$  mm, to the core, the lesser part flows, via pipeline  $D_{\text{pass}}70$  mm, to cool the lead target. The discharges for the core and lead target are 0,6 and 0,00662 kg/s, correspondingly. To regulate coolant discharge ratio for the core and lead target, regulatory valves (items A 1-1 and A 4-1) are installed at pipelines  $D_{\text{pass}}200$  mm and  $D_{\text{pass}}70$  mm. In case with tungsten target, the valve A 4-1 closes completely and the whole coolant flow for the core and tungsten target travels through pipeline  $D_{\text{pass}}200$  mm with a discharge rate 0,65 kg/s.

8.6 At the entrance to blanket housing, the pipeline  $D_{\text{pass}}200$  mm reduces to pipeline  $D_{\text{pass}}134$  mm and, further, to a rectangular box of cross-section  $440 \times 60$  mm. From the box, the coolant flows to upper collector of the core, then flows down in space between fuel elements and tungsten target, thus removing heat and cooling fuel elements and tungsten target. Coolant intended to cool the lead target flows, through pipelines  $D_{\text{pass}}70$  mm and  $D_{\text{pass}}24$  mm, to the lower collector of the target, and raises, through six U-shaped tubes, built in in target lead, along the target, then it flows down, thus cooling the target. Bottom ends of tubes are extracted to lower collector of the core, where coolant flows from the core and target get mixed and further removed as a joint flow, through rectangular box  $440 \times 60$  mm and pipelines  $D_{\text{pass}}134$  mm and  $D_{\text{pass}}200$  mm to heat exchanger 2-1.

8.7 Coolant temperature at output from the lower collector of blanket with tungsten target is  $88^{\circ}\text{C}$ , that with lead target is  $-93^{\circ}\text{C}$ . Pressure difference at the core with lead target is  $\sim 9,72\text{KPa}$ , at that with tungsten target is  $\sim 12,66\text{KPa}$ . After cooling, the coolant temperature in heat exchanger 2-1 is lowered up to  $\sim 40^{\circ}\text{C}$ . After

passing the heat exchanger 2-1, the coolant flows, through the pipeline  $D_{\text{pass}}200$  mm to the suck-in part of compressor.

8.8 At output pipeline between blanket and heat exchanger 2-1, coolant extraction and return pipelines of KGO system are inserted.

8.9 A pipeline  $D_{\text{pass}}25$  mm to clean the coolant (item 7 is ciolyte filter, items 8/1 and 8/2 are aerosol filters, items 9/1 and 9/2 are iodine filters) is cut in at pressure pipeline  $D_{\text{pass}}200$  mm. After cleaning, coolant is returned to loop 1 through pipeline  $D_{\text{pass}}25$  mm, which is cut in into suck-in pipeline  $D_{\text{pass}}200$  mm.

8.10 Coolant of loop 1 is cooled by removing heat in heat exchangers to the medium of loop 2, which is surrounding air, and surrounding air (air in the room) is cooled in water-air heat exchanger of loop 2. For this purpose, air cooling devices of loop 1 have built-in fans, which force cool room air along branchy external surface of heat exchanger and remove heat, cooling the heat exchanger of loop 1.

8.11 To cool the room air (loop 2), this air is forced, like in heat exchangers of loop 1, by built-in heat exchange fans of loop 2 along external surface of heat exchanger pipes and gives its heat to cold water, which comes to heat exchanger from cooling tower loop.

8.12 The cooling system is equipped with necessary means of monitoring and control.

