

# Results of CIEMAT simulations of SAD

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CIEMAT

- Target studies
- System static simulations
- System kinetic simulations
- Reactivity insertion and Dynamic tests

# SAD TARGET Simulations

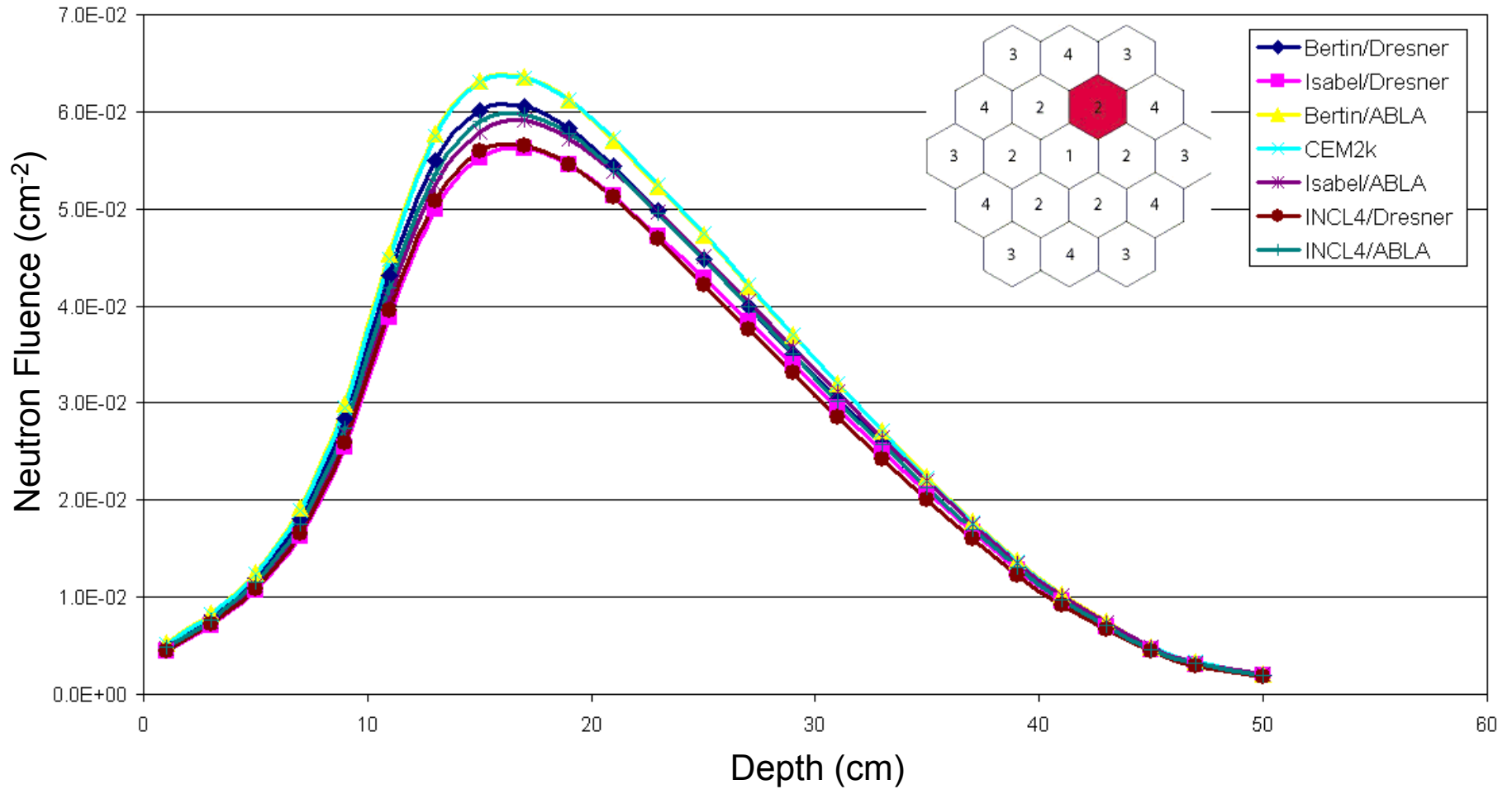
Up to 8 simulations had been performed with different high energy models using always the ENDFB6r6 data library and the MNCPx2.5e code

**Computed:** Neutron leakage, Neutron fluence, Energy deposition

Integrated number of neutrons per proton escaping from the lead target by the bottom, top and perimeter surfaces.

| Surface   | Bertin/Dresner | Isabel/Dresner | Bertin/ABLA | CEM2k              |
|-----------|----------------|----------------|-------------|--------------------|
| Bottom    | 5.3264E-01     | 4.8021E-01     | 5.7017E-01  | 5.5341E-01         |
| Top       | 1.9548E-01     | 1.9345E-01     | 2.0721E-01  | 1.9581E-01         |
| Perimeter | 1.2595E+01     | 1.1851E+01     | 1.3372E+01  | 1.3212E+01         |
| Surface   | Isabel/ABLA    | INCL4/Dresner  | INCL4/ABLA  | INCL4/ABLA updated |
| Bottom    | 5.1212E-01     | 5.1212E-01     | 4.8130E-01  | 5.18822E-01        |
| Top       | 2.0438E-01     | 2.0438E-01     | 1.7675E-01  | 1.88195E-01        |
| Perimeter | 1.2552E+01     | 1.2552E+01     | 1.1761E+01  | 1.25800E+01        |

The deviations between different physics models in both tables range from 13% to 17%.



Neutron flux depth dependence for the cell #2 of the target

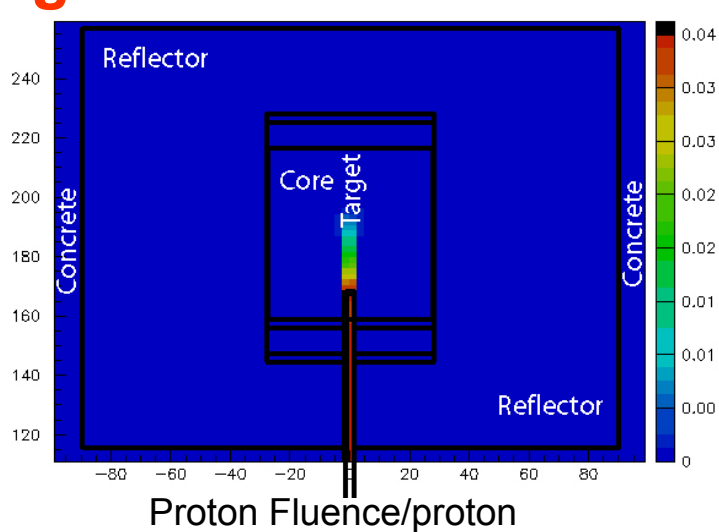
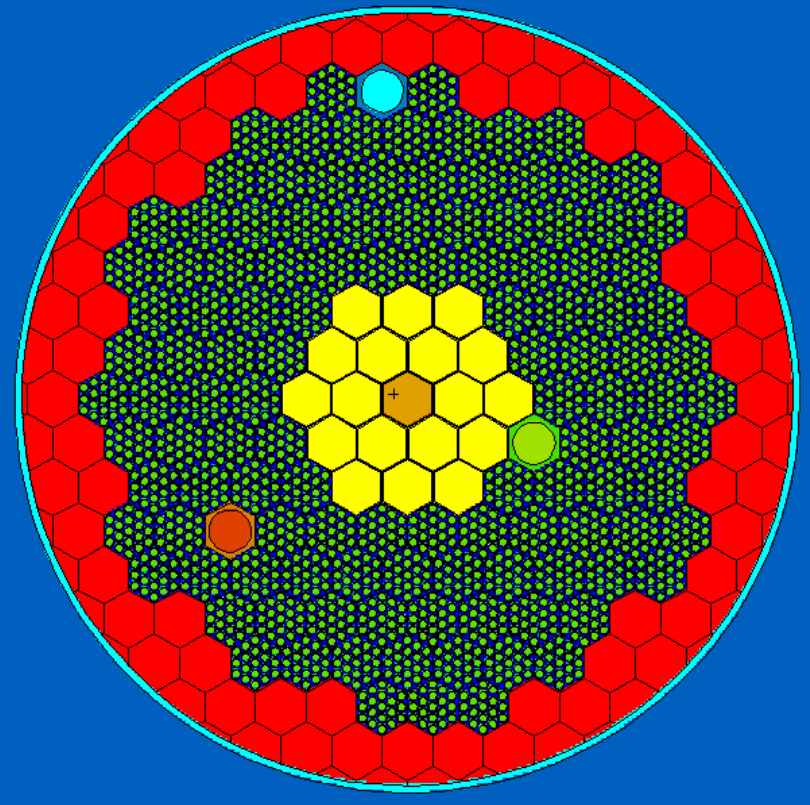
# System static simulations

More than 20 simulations

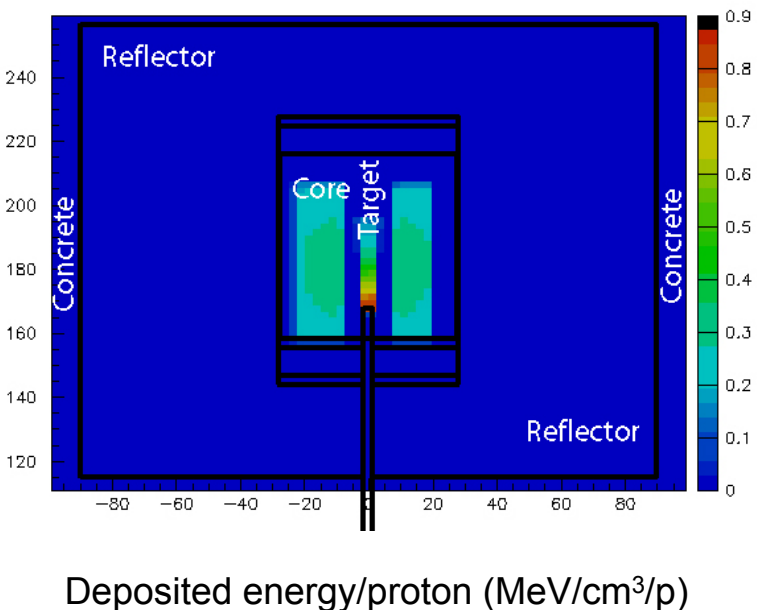
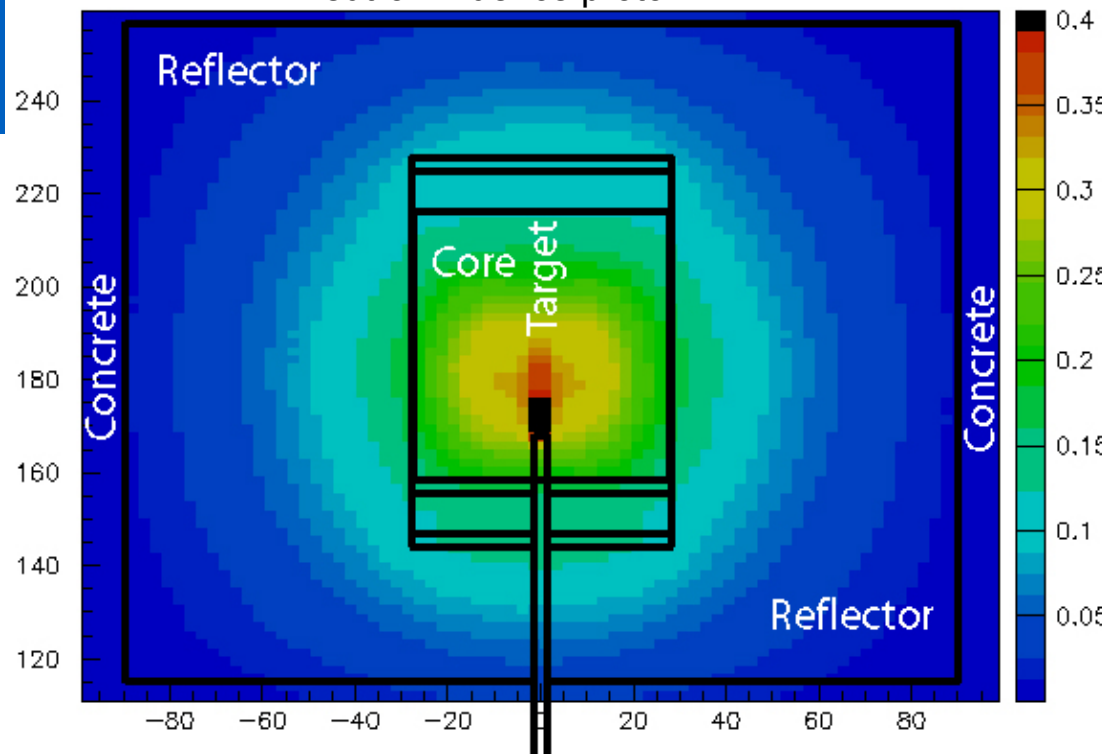
$K_{\text{eff}}$ , Spatial distributions of neutron and proton fluence and Energy deposition

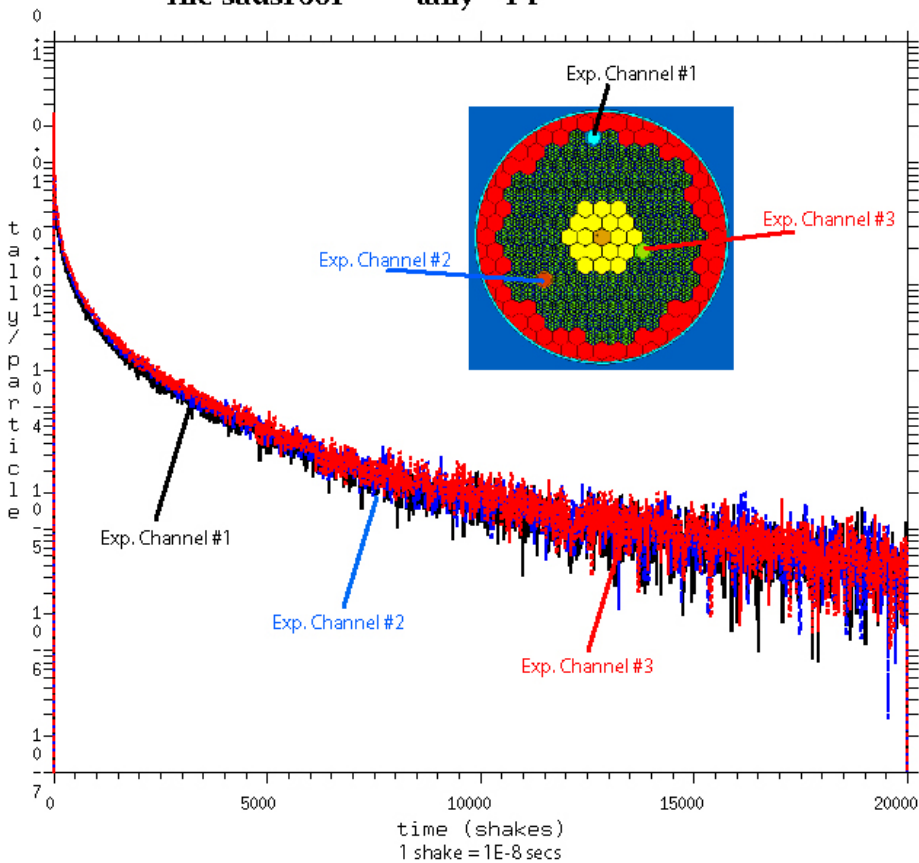
| Case number | New radius of the lead reflector | Number of fuel assemblies removed/Total | Modification   | $K_{\text{eff}} \pm \text{Error}$ |
|-------------|----------------------------------|---|--|-----------------------------------|
| 1           | Without modification             | none/145                                | none   | $0.94951 \pm 0.00036$             |
| 2           | ~60cm                            | none/145                                | none   | $1.00726 \pm 0.00101$             |
| 3           | ~70cm                            | none/145                                | none   | $1.01352 \pm 0.00112$             |
| 4           | ~80cm                            | none/145                                | none   | $1.01937 \pm 0.00120$             |
| 5           | ~60cm                            | 4/141                                   | none   | $1.00177 \pm 0.00112$             |
| 6           | ~60cm                            | 8/137                                   | none   | $0.99434 \pm 0.00109$             |
| 7           | ~60cm                            | 12/133                                  | none   | $0.98328 \pm 0.00105$             |
| 8           | ~60cm                            | 16/129                                  | none   | $0.97541 \pm 0.00113$             |
| 9           | ~60cm                            | 20/125                                  | none   | $0.96608 \pm 0.00102$             |
| 10          | ~60cm                            | 24/121                                  | none   | $0.95416 \pm 0.00110$             |
| 11          | ~60cm                            | 28/117                                  | none   | $0.94386 \pm 0.00098$             |
| 12          | ~60cm                            | 26/119                                  | none   | $0.94783 \pm 0.00010$             |
| 13          | ~70cm                            | 26/119                                  | none   | $0.95150 \pm 0.00010$             |
| 14          | ~80cm                            | 26/119                                  | none   | $0.95425 \pm 0.00011$             |
| 15          | ~60cm                            | 26/119                                  | 10% of B-10 to the first 10 cm of of concrete close to lead reflector                                | $0.94195 \pm 0.00011$             |
| 16          | ~60cm                            | 24/121                                  | Idem as case #15   | $0.95027 \pm 0.00011$             |
| 17          | ~60cm                            | 25/120                                  | Idem as case #15   | $0.94563 \pm 0.00011$             |
| 18          | ~60cm                            | 22/123                                  | 0.5% of $^{10}\text{B}$ @ internal lead reflector<br>1.0% of $^{10}\text{B}$ @ bottom and top plates | $0.95089 \pm 0.000108$            |
| 19          |                                  |   | Latest SAD MCNP Input distributed  | $0.94627 \pm 0.00101$             |

# Configuration number #12



Neutron Fluence/proton

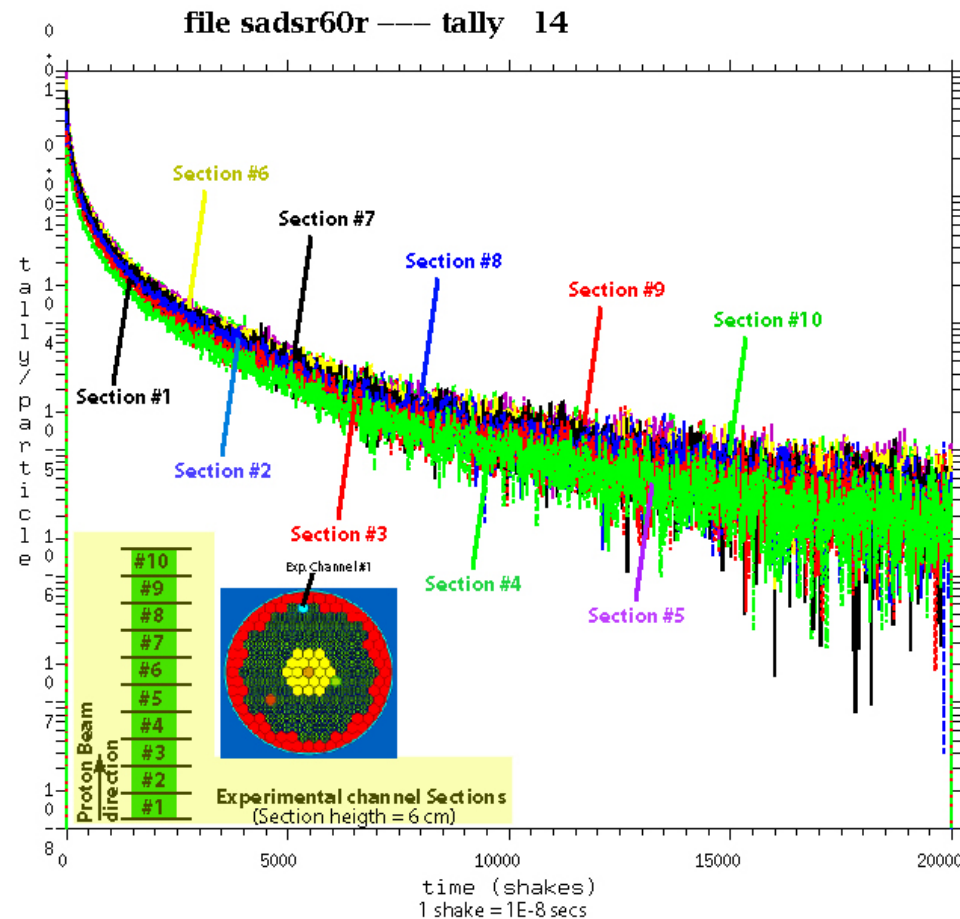


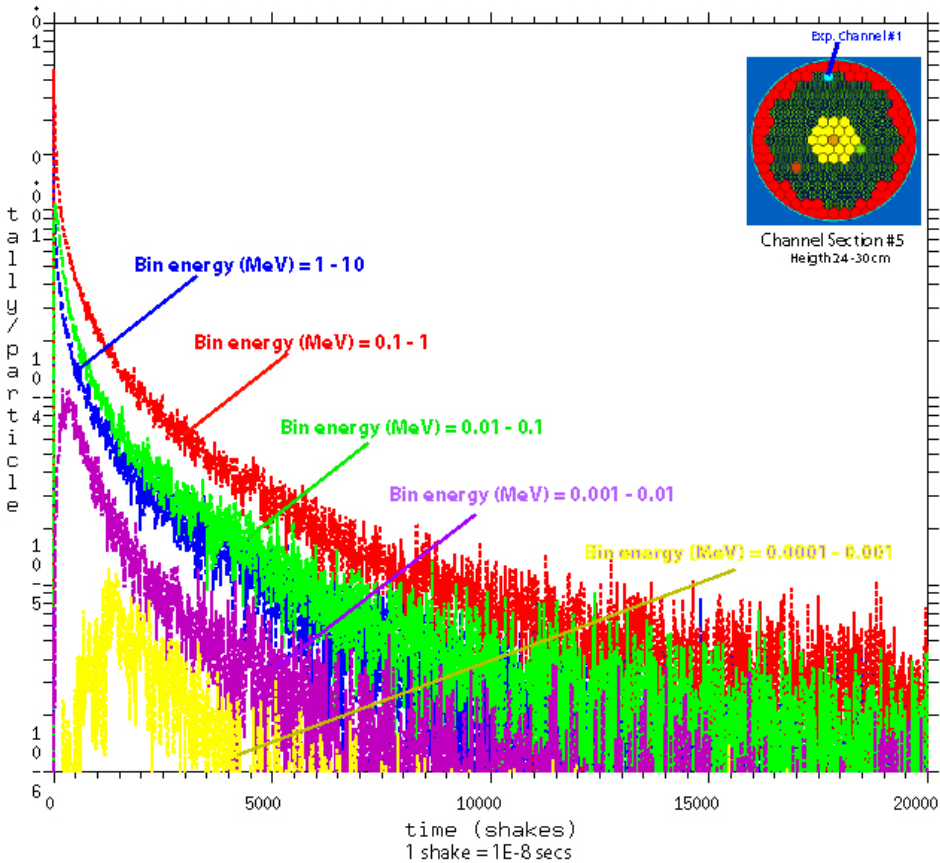


Case #12: Time evolution of  $^{235}\text{U}$  fission counting rate. Central height.  
Detectors in the 3 experimental channels at the core.

## System kinetic simulations

Case #12: Time evolution of  $^{235}\text{U}$  fission counting rate. Exp. Channel 1 in the core.  
Detectors at 10 different heights.

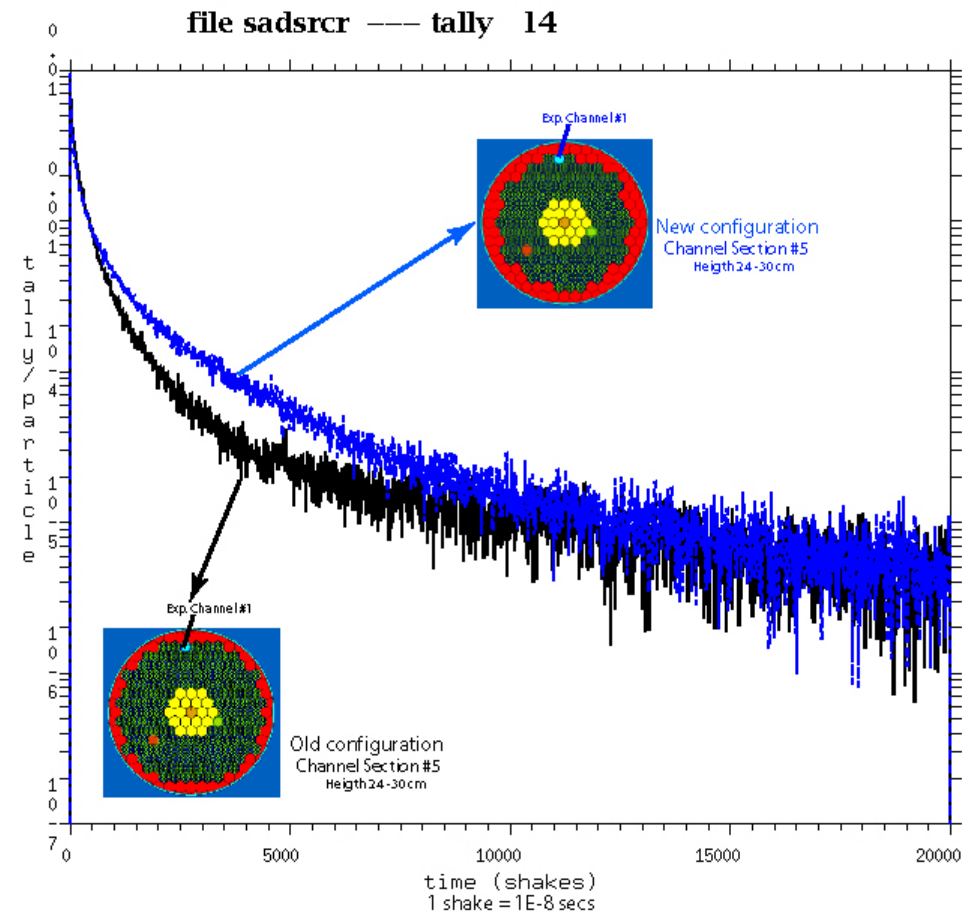


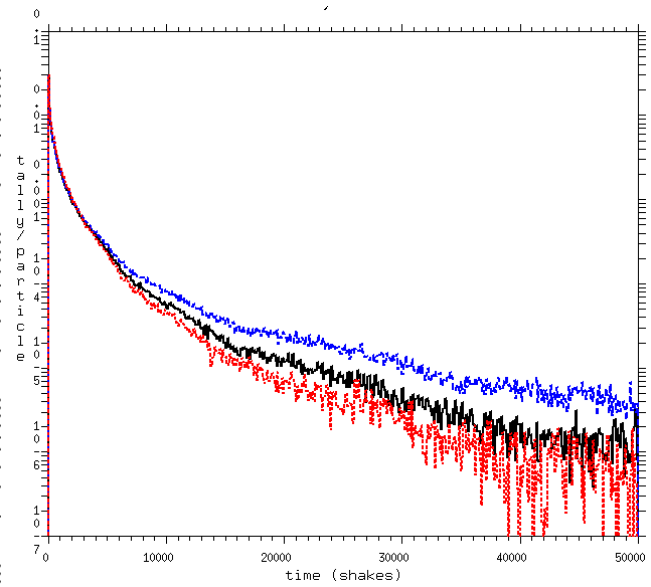
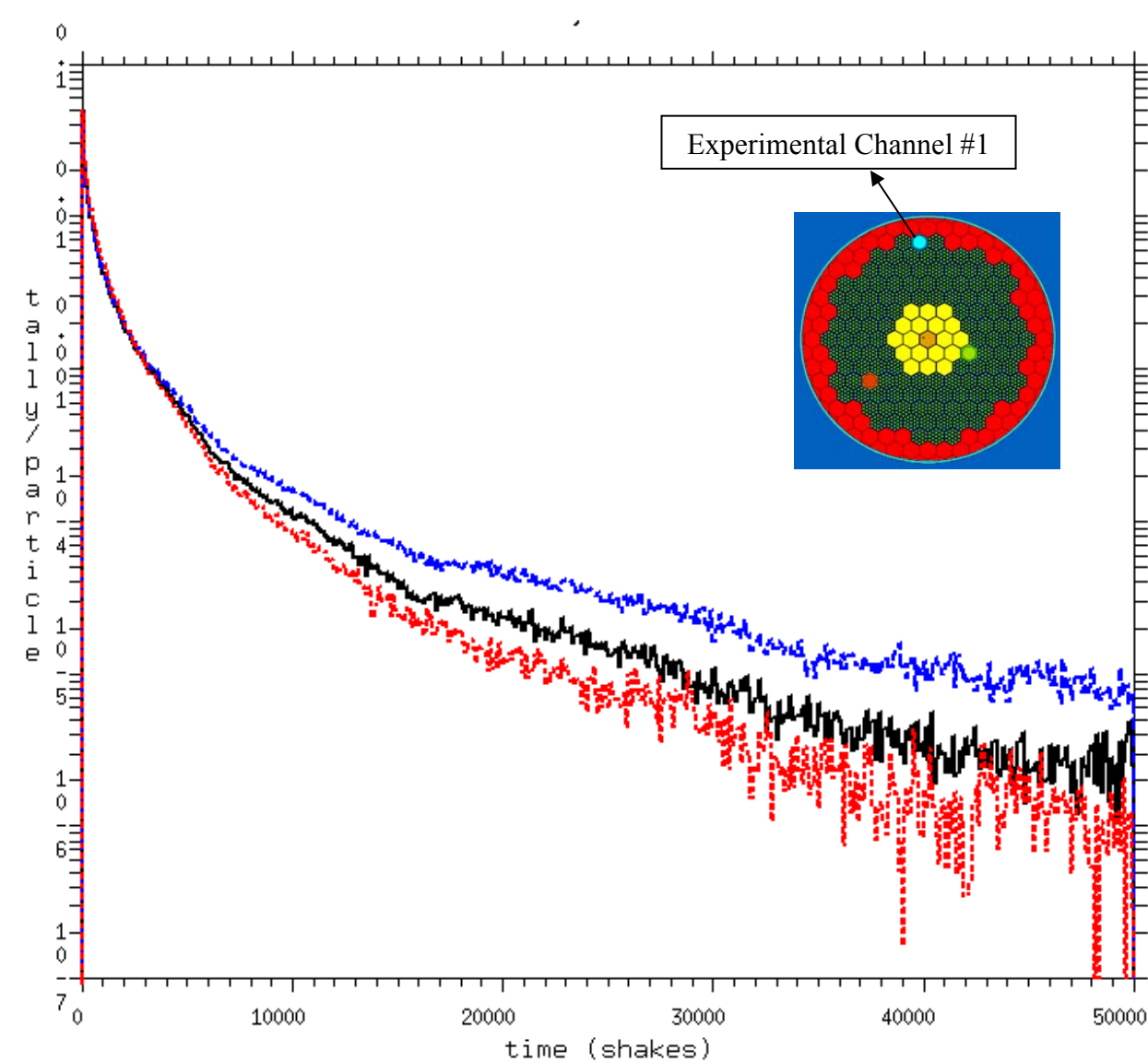


Case #12: Time evolution of  $^{235}\text{U}$  fission counting rate. Exp. Channel 1 in the core. Central height.  
Contributions from different energy intervals

## System kinetic simulations

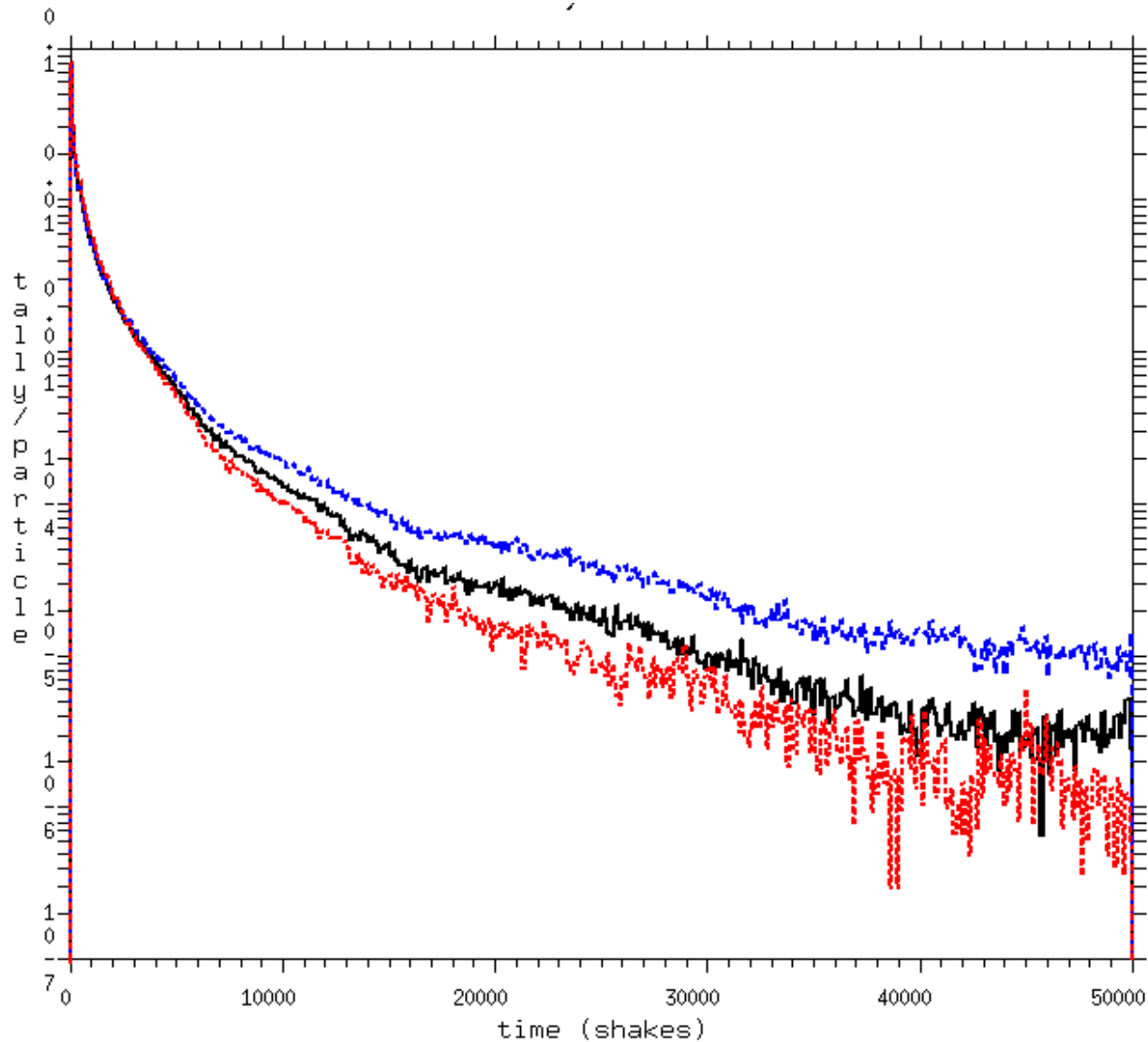
Time evolution of  $^{235}\text{U}$  fission counting rate. Exp. Channel 1 in the core. Central height. Case #1(0.94951) vs. Case #12 (0.94783).





Energy interval between 0.1 MeV and 1 MeV

Neutron time response in the **experimental channel #1** at central height. Virtual  $^{235}\text{U}$  fission detectors were placed in the center of the experimental channel.  
**Blue** = Case #12; **Black** =Case #15 (Borated Concrete); **Red**=Case #18 (Borated Pb)



Neutron time response in the external experimental channel placed in the **lead reflector** ( $R=40.5\text{cm}$ ) at central height.

Virtual  $^{235}\text{U}$  fission detectors in the center of the experimental channel.

**Blue** = Case #12; **Black** =Case #15 (Borated Concrete); **Red**=Case #18 (Borated PB)

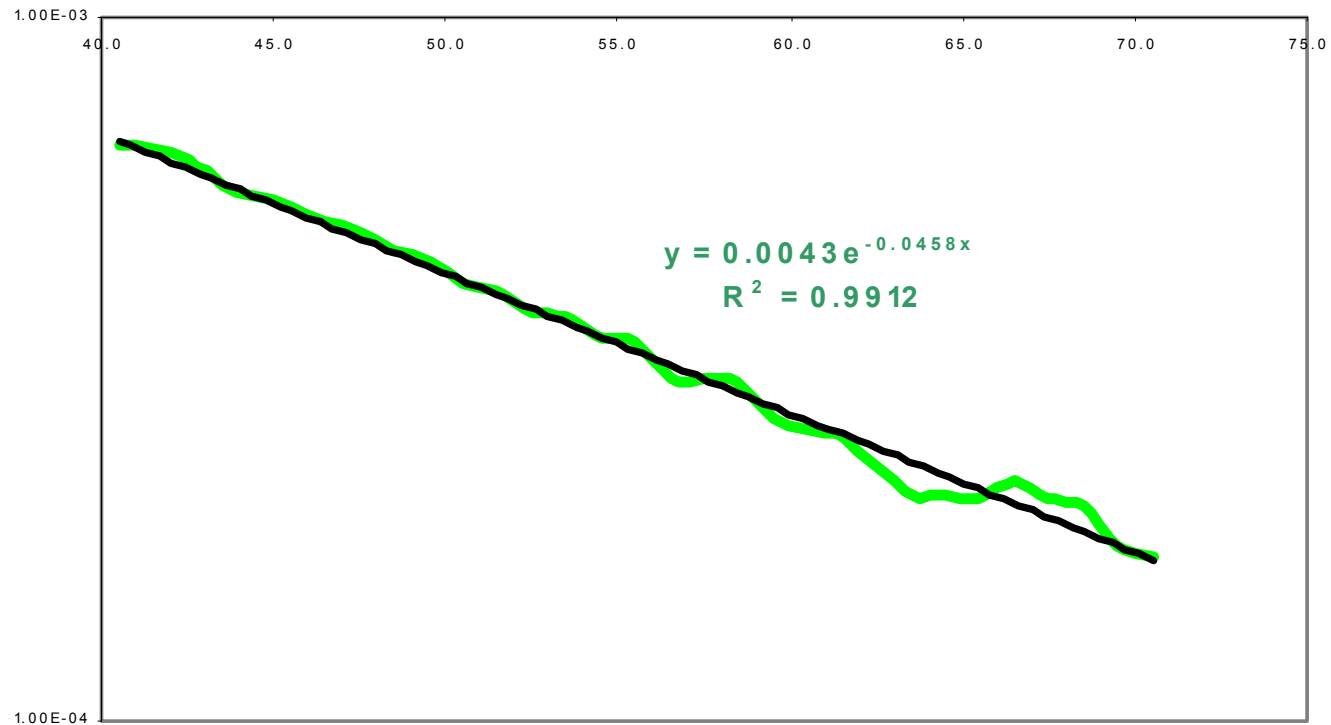
Application of simple point kinetics to case #18:

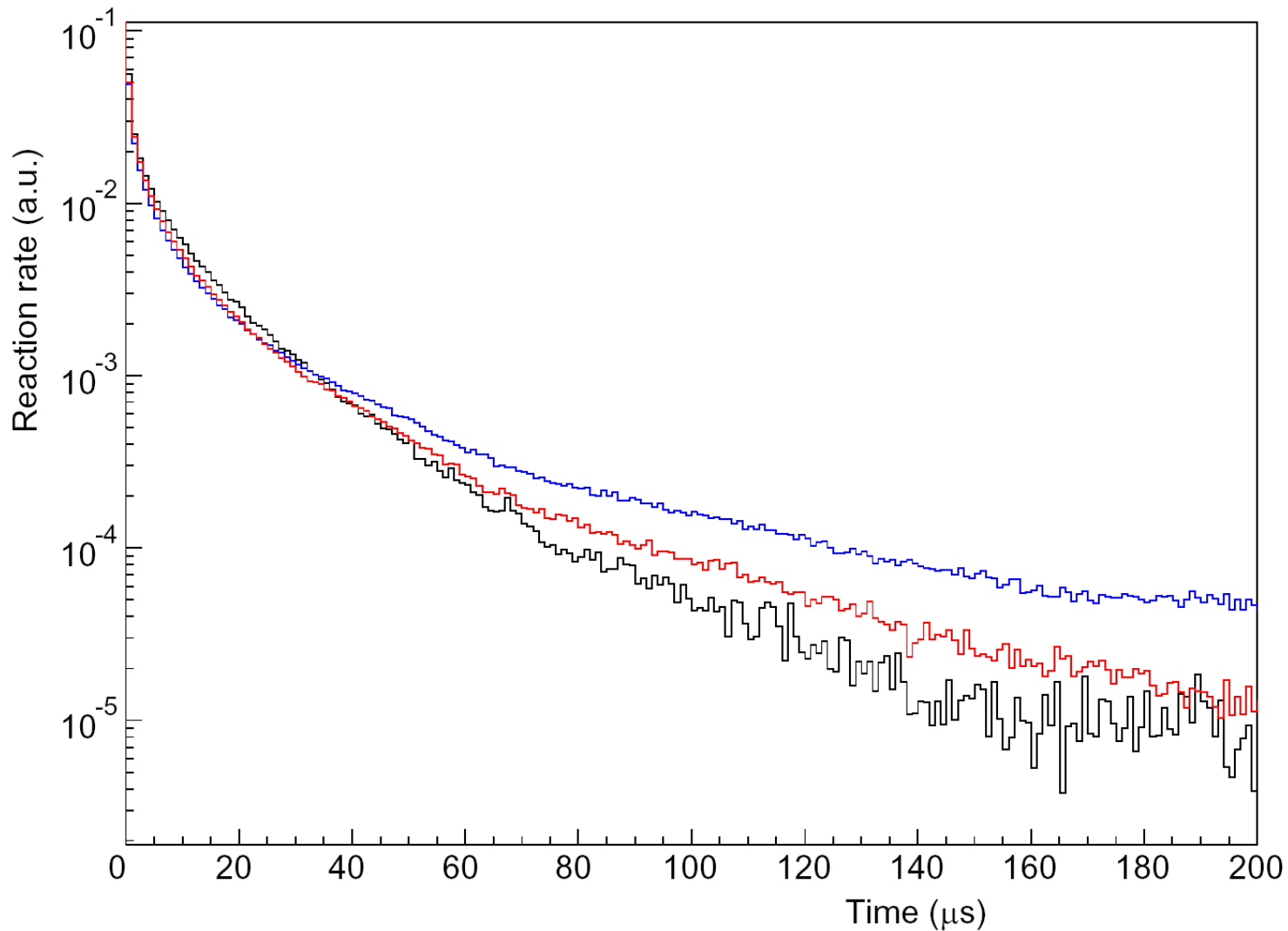
MCNP:  $\Lambda=9.543 \cdot 10^{-7}\text{s}$  ,  $\beta=345 \text{ pcm}$ ;

FIT:  $\alpha=45800 \text{ s}^{-1}$

then,  $\rho(\$) = 11.6$  so  $K_{\text{eff}} = 0.9597$

Note:  $\beta_{\text{eff}}$  Case #1 =  $368 \pm 10$  (pcm)  
 $\beta_{\text{eff}}$  Case #12 =  $350 \pm 10$  (pcm).





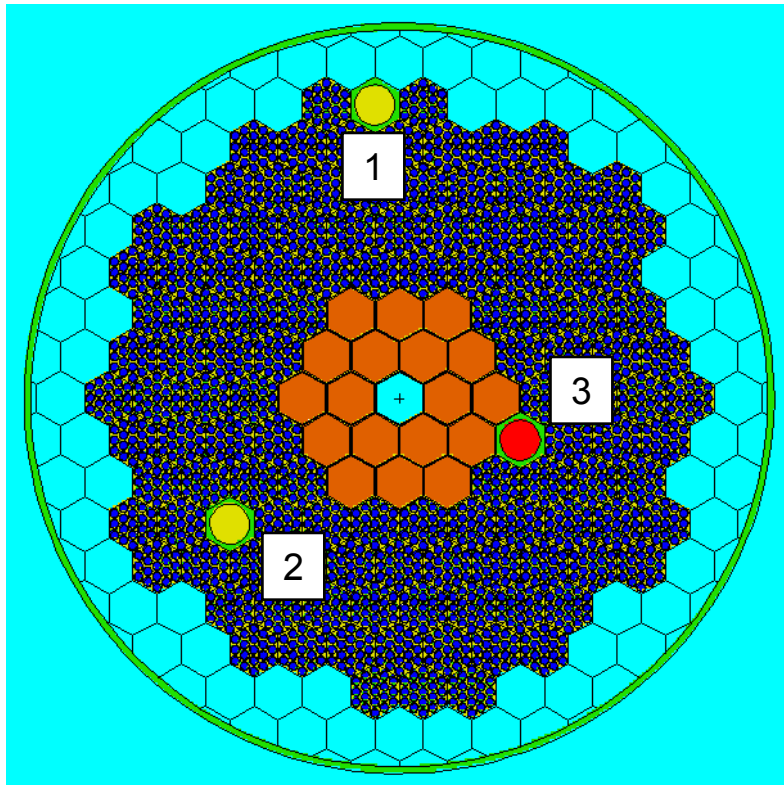
Neutron time response in the **experimental channel #1** at central height.

Virtual  $^{235}\text{U}$  fission detectors were placed in the center of the experimental channel.

**Blue** = Case #12; **Red**=Case #18 (Borated PB); **Black** =Case #19 (Latest SAD Distr. Input file)

# Reactivity insertion simulations

Introduction of a  $B_4C$  cylinder ( $\varnothing 3$  cm  $\times$  51 cm long)  
in the core experimental channels



| $K_{\text{eff}}$ reference = 0.94783 |                  |                         |
|--------------------------------------|------------------|-------------------------|
| Exp. Channel                         | $K_{\text{eff}}$ | $\Delta k_{\text{eff}}$ |
| 3                                    | 0.92406          | -0.02377                |
| 2                                    | 0.92720          | -0.02063                |
| 1                                    | 0.93063          | -0.01720                |

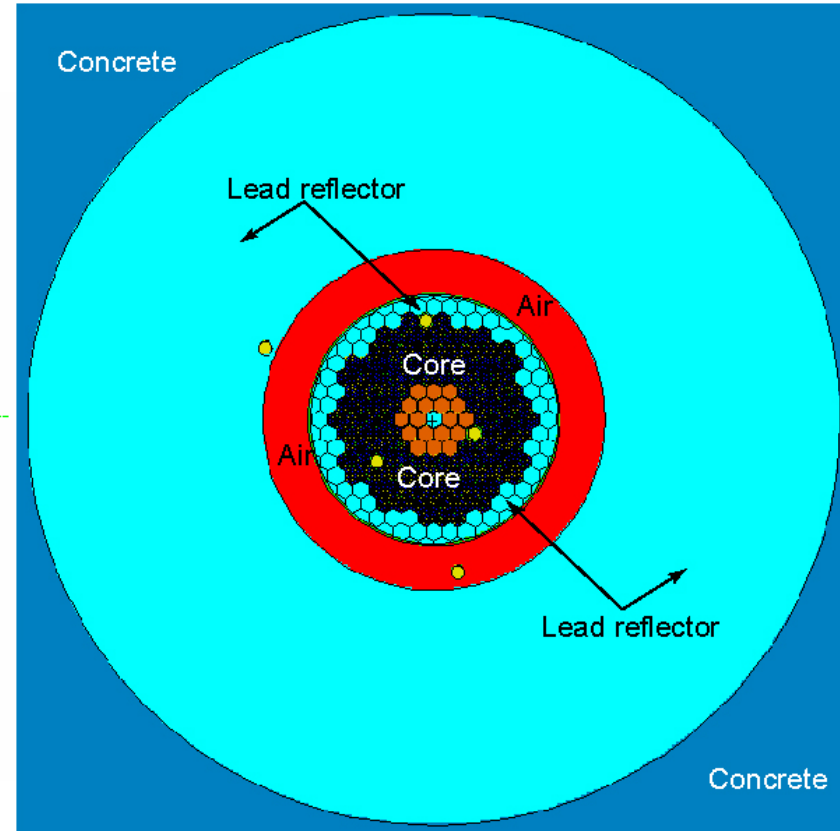
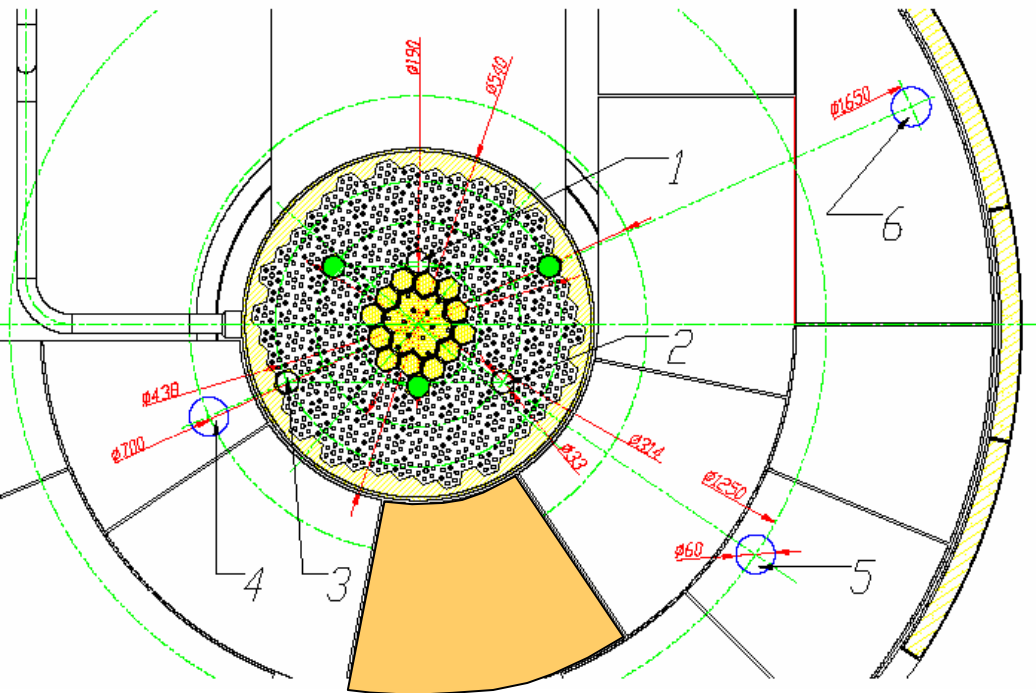
# Reactivity insertion simulations

## Reduction of the reflector effect:

- In reality extraction of one of the reflector elements.
- In the simulation reduction of the lead thickness.

$$K_{\text{eff}} \text{ reference} = 0.94783$$

| Reduct. of $\varnothing$ cm | $K_{\text{eff}}$ | $\Delta k_{\text{eff}}$ |
|-----------------------------|------------------|-------------------------|
| 20                          | 0.84882          | 0.09901                 |
| 6                           | 0.91437          | 0.03346                 |



# Dynamic tests proposal

In the near future (<7 years) there will be no ADS system that

- Is similar to the proposed transmutation device: Fuel, Coolant, Neutron Spectrum
- and Has sufficient power / heaters as to introduce significant thermal feedbacks

Two complementary approaches:

- 1) Use a different system with significant feedbacks (TRADE-Plus)
- 2) Use a similar ADS system simulating the feedbacks ( ⇒ **SAD** )

*The proposal is to study dynamic feed-backs of ADS systems by artificial introduction of reactivity variations following the pattern of the calculated thermal feedbacks in industrial ADS incidents.*

The reactivity (positive/negative) insertions can be obtained by programmed reflector movements (more complicated options possible).

The follow up can be done by neutronic detectors, and actions can be applied by beam actuation or absorbers in the experimental channels.

It would be interesting to study insertions of as much as  $\pm 1000$  pcm (from  $0.95 \rightarrow 0.96$  and from  $0.95 \rightarrow 0.94$ ).

# Conclusions

15% differences are observed on the neutron production/proton from different nuclear models in the target simulation

Large lead reflector:

- Reduce the number of fuel elements / fissile material (margin to increase  $K_{\text{eff}}$ )
- Recover a kinetic behavior closer to point kinetics
- Low energy neutron absorber ( $^{10}\text{B}$ ,  $^6\text{Li}$ , Cd) around core improve kinetic response
- Attention to absorbing materials in the reflector

Kinetic techniques might be usable at SAD for reactivity determination

Large reactivity insertions can be obtained by:

- Reflector modification
- Absorber rods ( $\text{B}_4\text{C}$ ) on the experimental channels
- Need of electromechanical fast actuators

These options might allow investigation of ADS dynamic behavior

SAD might allow to study: Source multiplication, source importance, Shielding aspects, and other static effects but probably also **kinetic and dynamic ADS aspects**